

The Development and Verification of a Novel **M**odular **A**ir **C**ooled **C**ondenser for Enhanced Concentrated **S**olar Power Generation

ACC Users Group 5<sup>th</sup> Annual Meeting  
October 16<sup>th</sup>, 2013

*“Performance Characteristics of a Novel  
Modular Air-Cooled Condenser”*

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UNIVERSITY of LIMERICK

OLLSCOIL LUIMNIGH

# Presentation Overview

- Project Background
- Objectives
- Current Practice in ACCs
  - Measurements on Conventional A-Frame ACC in Ireland
- Modular ACC (MACC) Design
- Experimental Measurements on MACC Prototype
  - Air-side characterisation
  - Steam-side characterisation
- Impact on Plant Output
- Current Work

# Project Background

- In March 2007 the EU committed to source 20% of Europe's electricity from renewable sources by 2020
  - Concentrated Solar Power (CSP) is forecasted to provide 25% of this target
  - 630,000 TWh/y of solar radiation falls on the Mediterranean region (Europe consumes just 4,000 TWh/y ~0.6% of available energy)









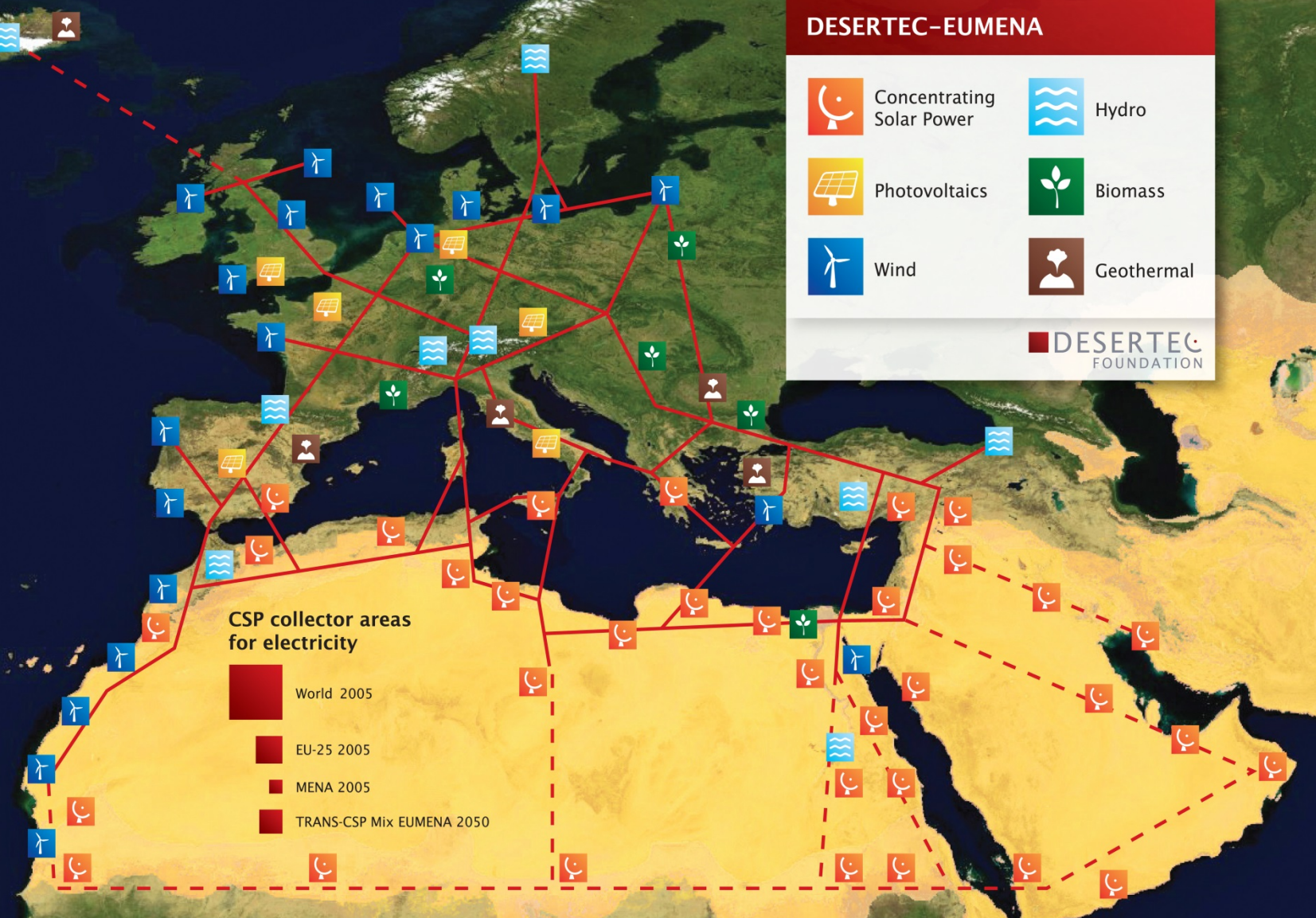
# DESERTEC-EUMENA

	Concentrating Solar Power		Hydro
	Photovoltaics		Biomass
	Wind		Geothermal



**CSP collector areas for electricity**

	World 2005
	EU-25 2005
	MENA 2005
	TRANS-CSP Mix EUMENA 2050



# Project Background

- CSP development is being prioritised by EU
- Barriers to maximising CSP potential
  - Absence of cooling water for condensers in Rankine Cycle
  - Inefficiency of current air-cooling methodologies



- According to the European Strategic Energy Technology (SET) plan a 25% loss in CSP plant output can occur on warm days



# Project Background

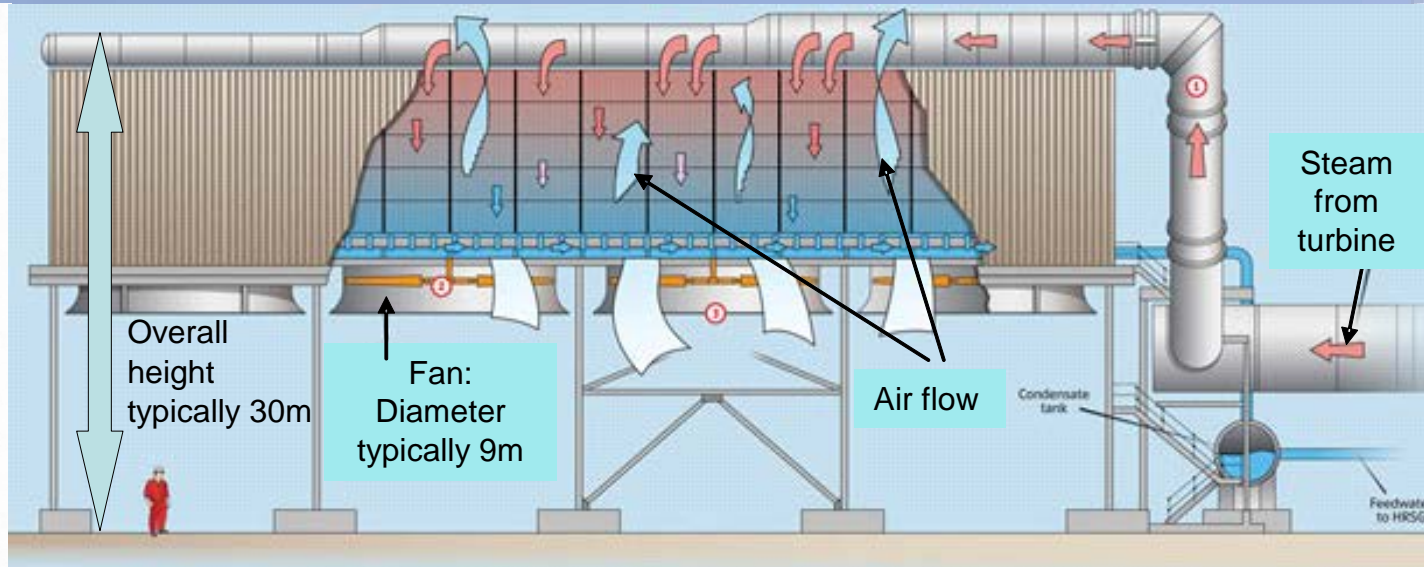
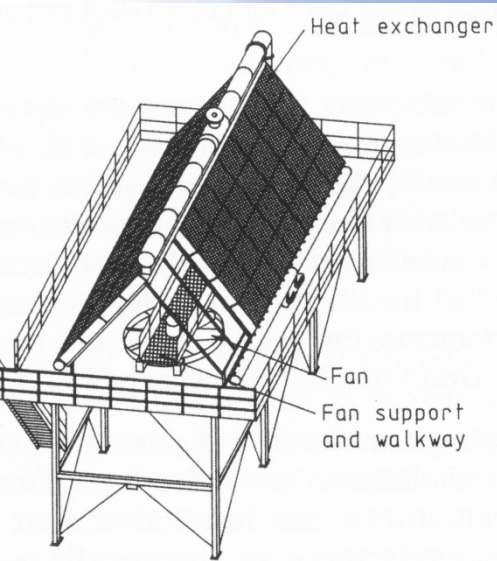
- For successful deployment of CSP, enhanced air-cooling methodologies must be developed
- Seventh EU Framework programme (FP7) provides funding to successful project proposals
- MACCSol secured €7m funding in 2010
  - Consortium consists of 3 universities and 5 industrial partners



# Objectives

- High level objectives:
  - Facilitation of EU's 2020 renewable energy target
  - Ensure successful deployment of CSP
  - Elimination of water for cooling CSP condensers
  - Minimise inefficiencies and losses associated with current ACCs
  - Maximise power output from air-cooled CSP plants
  - Ensure CSP is cost-competitive with fossil-fuel based power generation

# Current Practice in ACCs

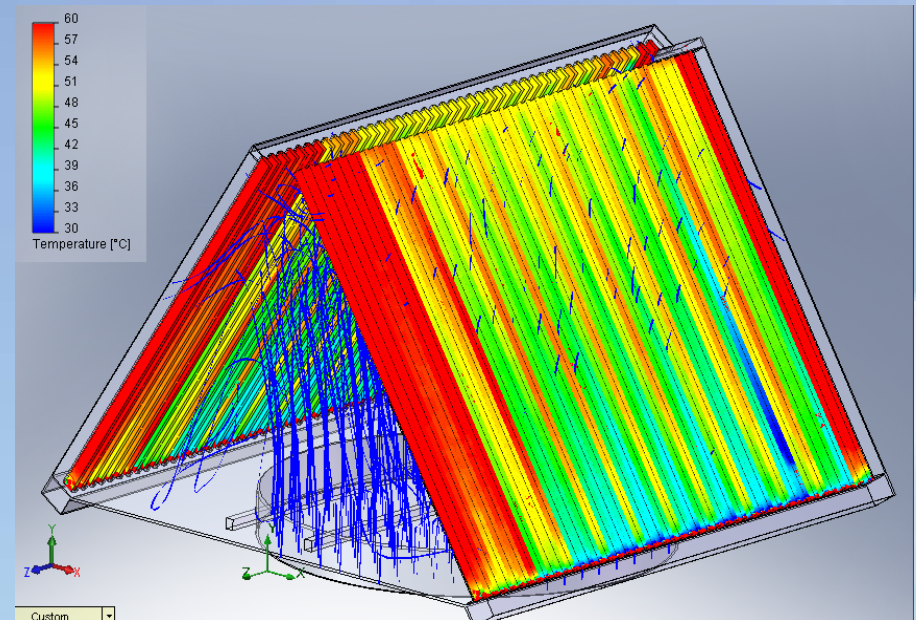
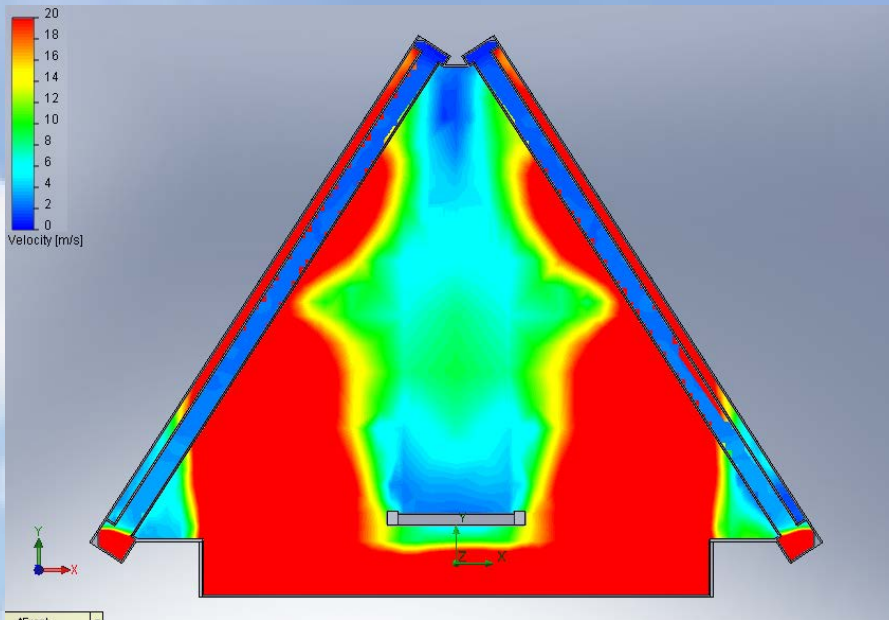


- Large diameter fans are typically two-speed
  - Since the fans are switched in steps, certain deviations upward or downward from the desired set point are unavoidable
- Fans typically consume 150kW
  - 20 fans for 150 MW plant (Irish Power Plant)
  - $20 \times 150\text{kW} = 3\text{MW} = \underline{2\% \text{ of plant output}}$
- Large structures are costly to erect
  - High strain rates can eventually lead to failure



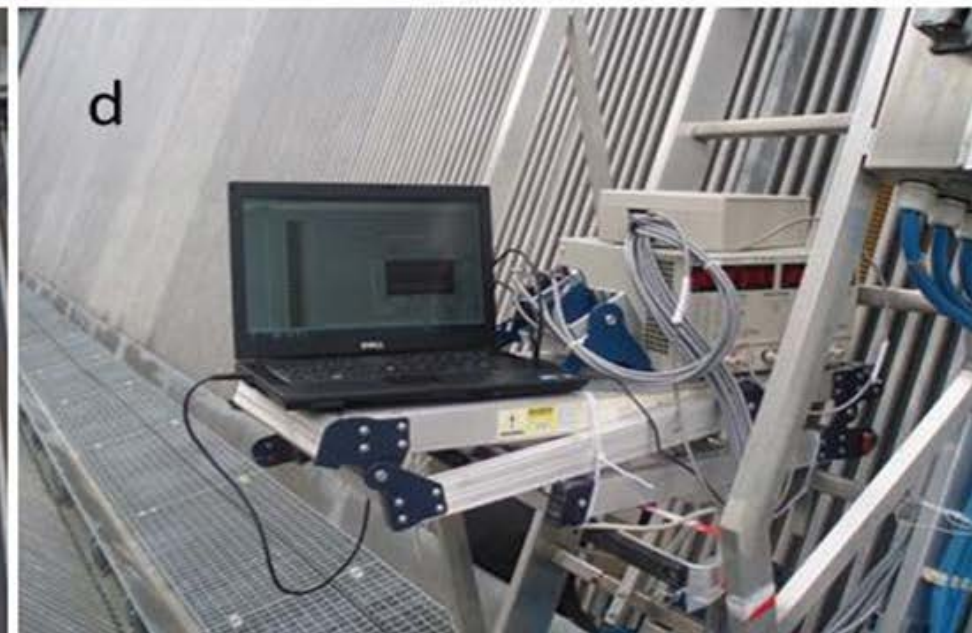
# Current Practice in ACCs

- Suspect to wind effects
- Highly non-uniform flow distribution on air-side



- Lack of quantitative data available in public domain
  - Flow distribution measurements carried out on A-Frame ACC in a ~400MW plant in Ireland

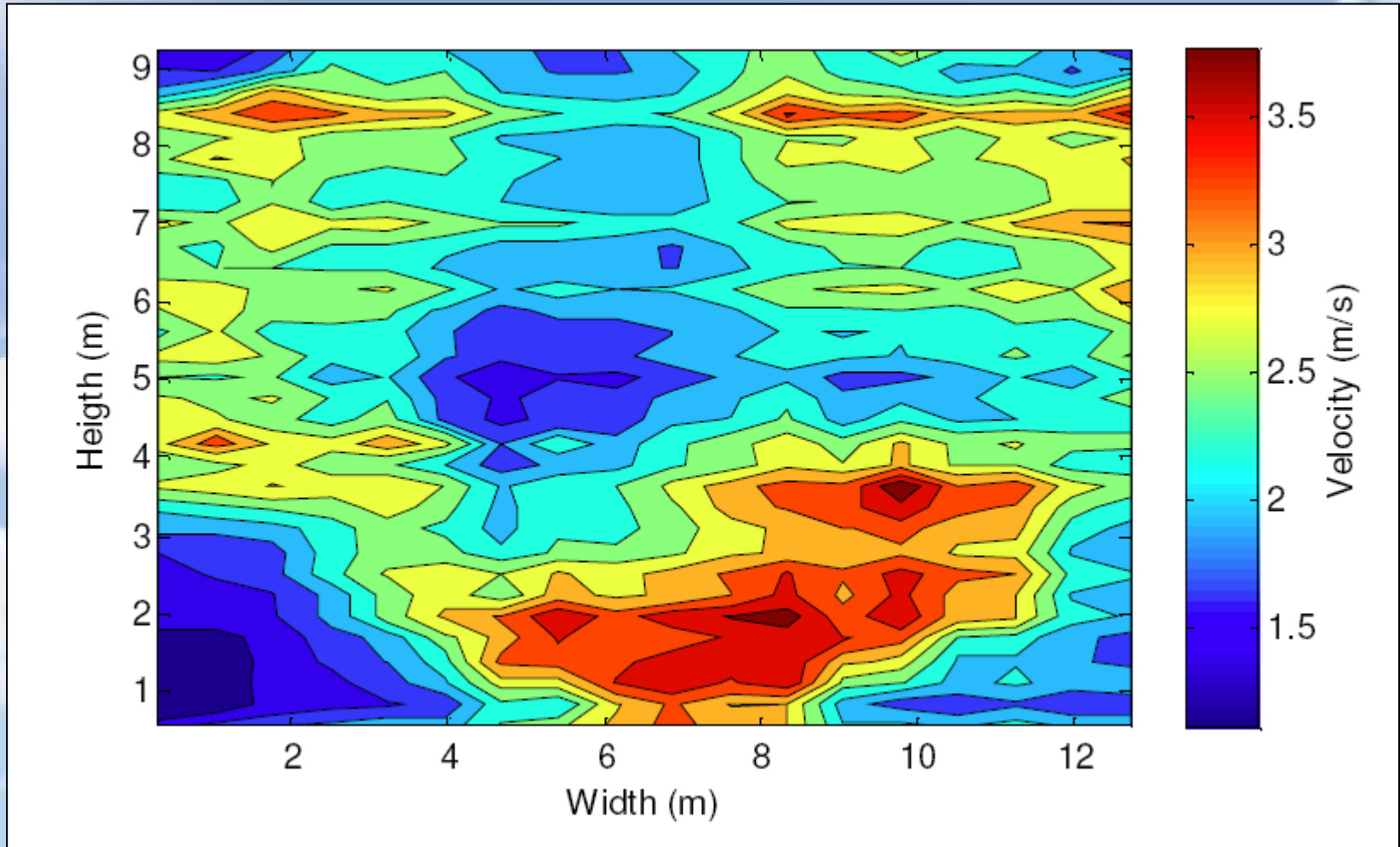
# Measurements on Conventional ACC





# Measurements on Conventional ACC

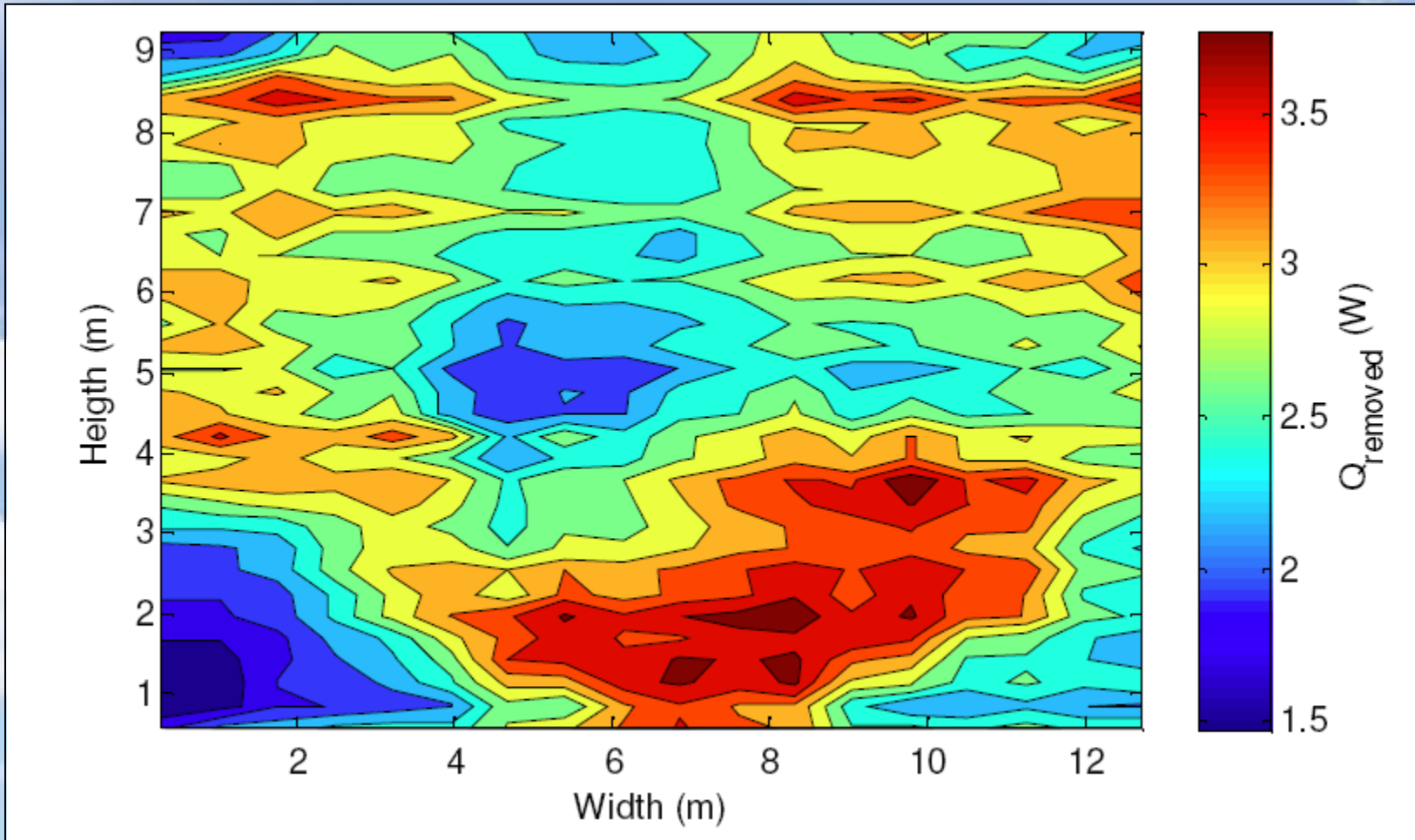
- Exit velocity field from ACC cell with single ACC fan operational





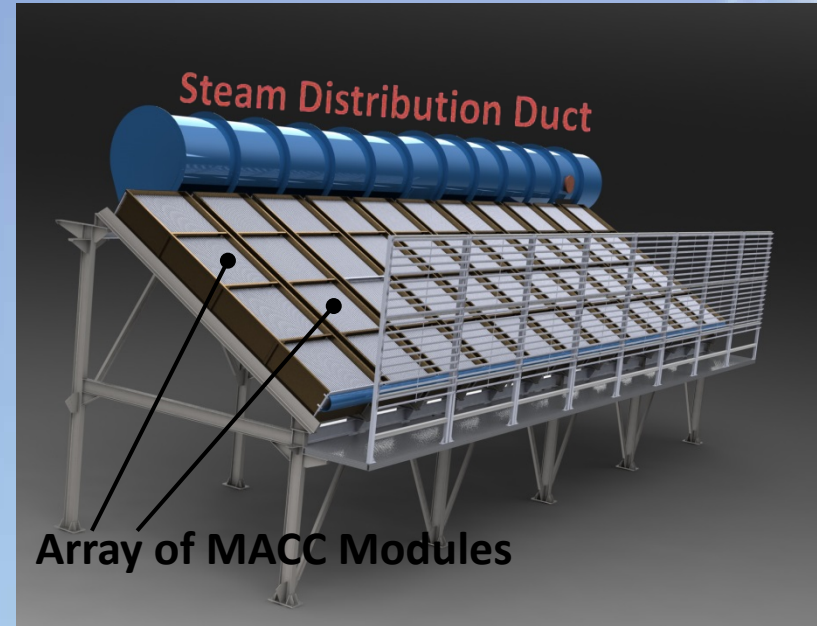
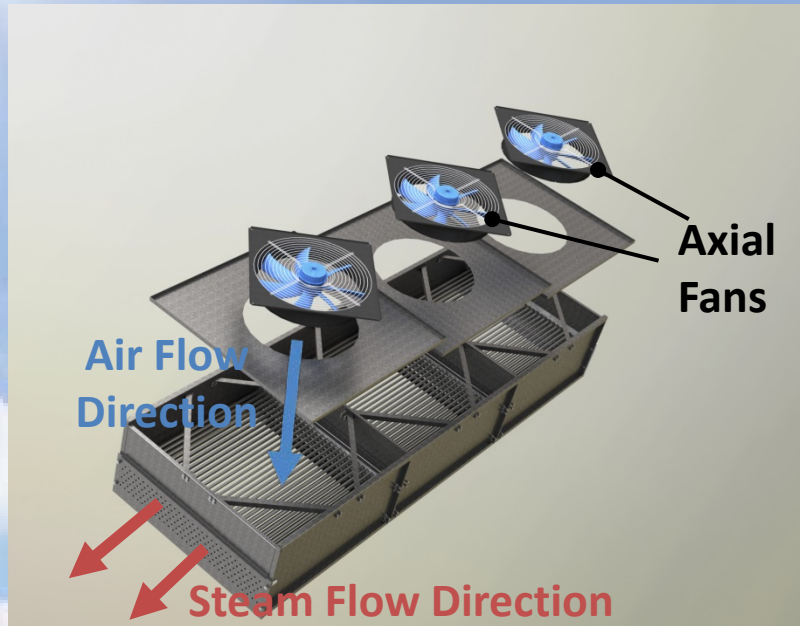
# Measurements on Conventional ACC

- Heat removal rate from ACC cell with single fan operational



# Modular ACC Design

- Modular Air Cooled Condenser – MACC

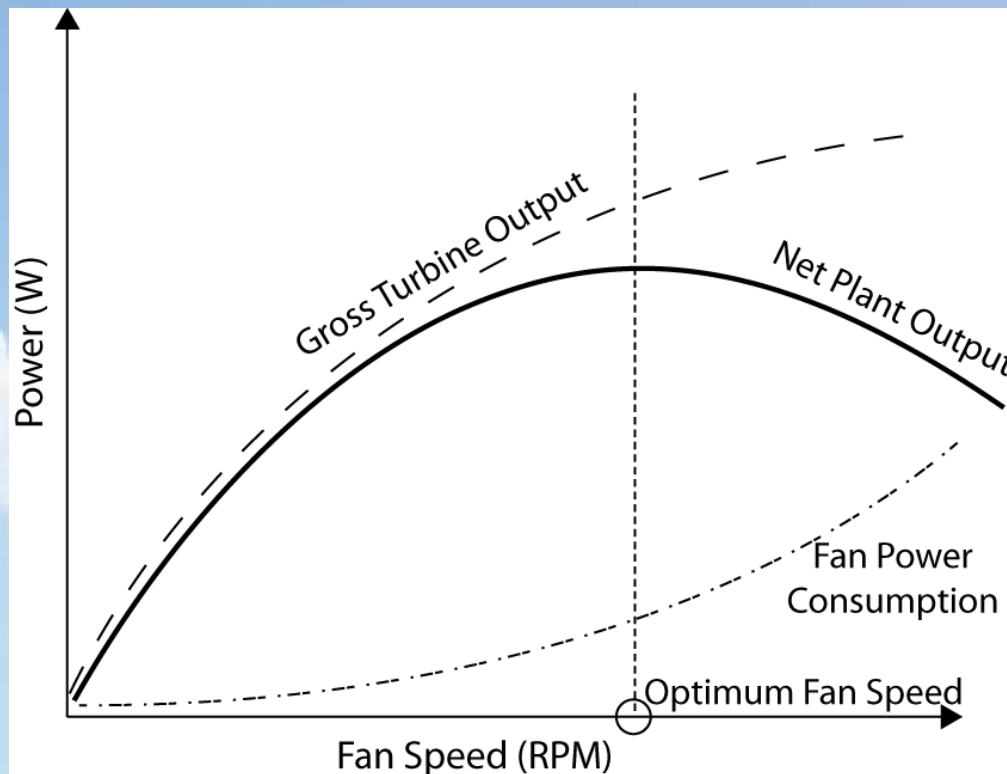


- Modular nature – reduced transport, installation & maintenance costs
  - Beneficial for difficult-to-reach places such as desert CSP sites
- Close proximity of small fans to heat exchanger core ensures uniform air flow over the entire tube bundle

**MACCsel** “Dead-zones” arising from flow maldistribution are eliminated

# Modular ACC Design

- MACC design incorporates small, speed controllable electric fans
  - Fan speed is continuously variable to maintain optimum condenser conditions irrespective of ambient temperature or steam turbine load
    - Sensors and feedback loop create control algorithm for fans
  - Ability to achieve and maintain an **optimum operating point**
  - Maximise plant output without over-consumption of fan power

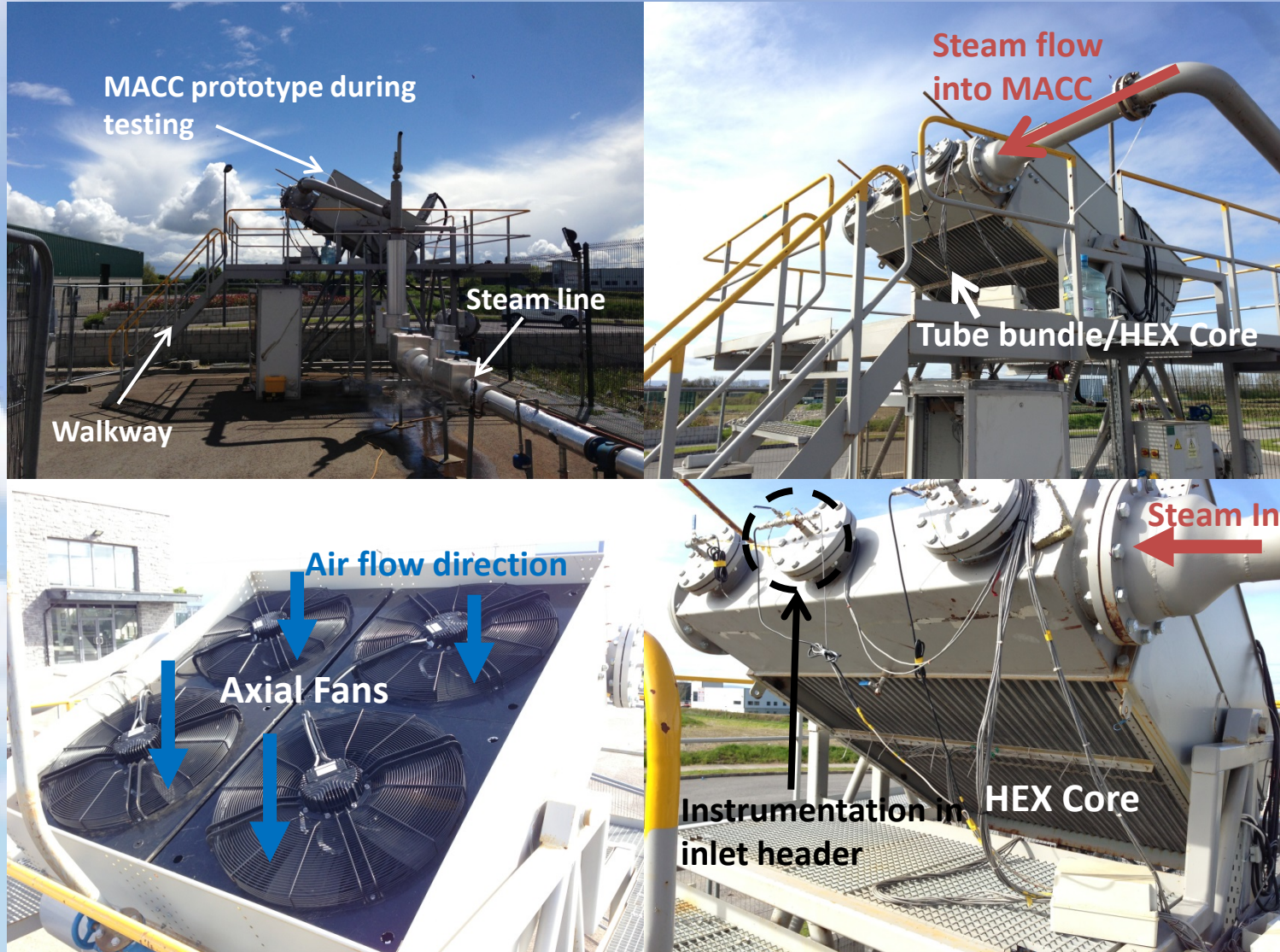


$$\text{Net Power} = \text{Gross Power} - \text{Fan Power}$$



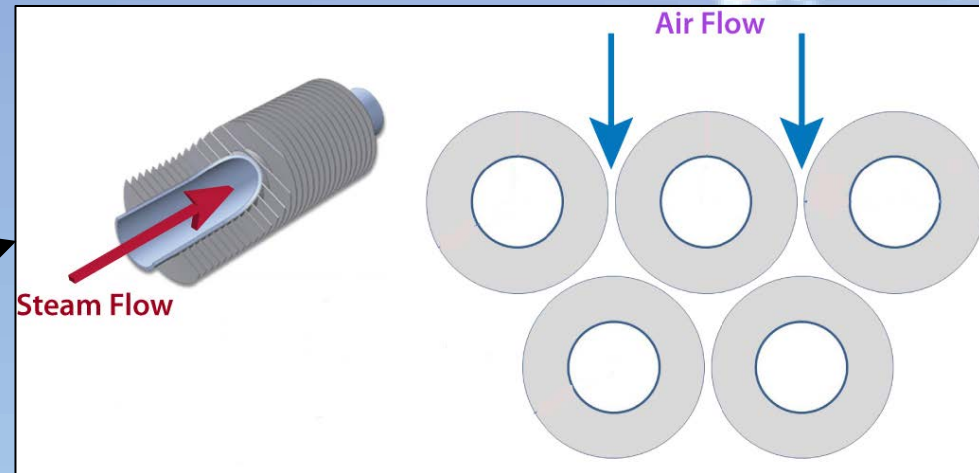
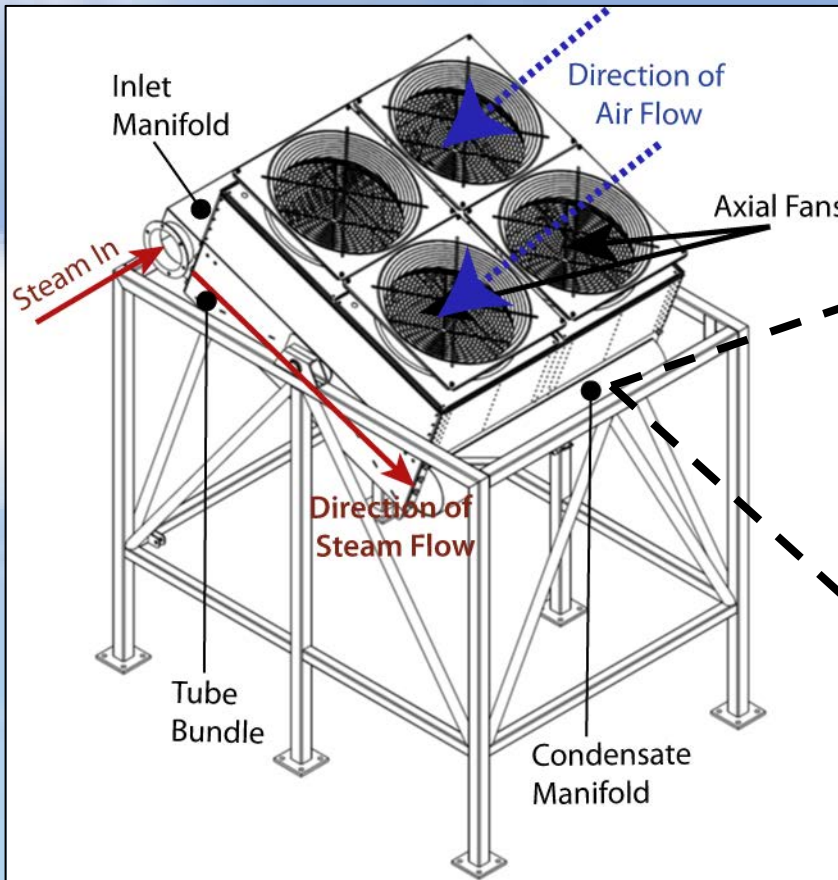
# Modular ACC Design

- Full-scale prototype designs have been fabricated and tested on-site in Ireland

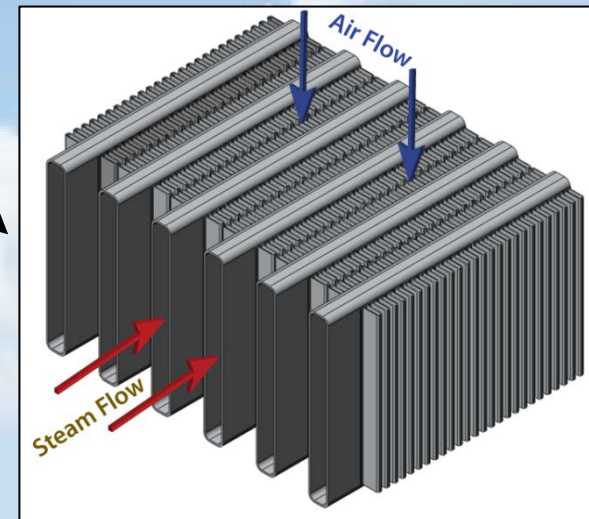


# Modular ACC Design

- 3 compact heat exchanger designs have been characterised
  - 6 row circular-finned heat exchanger
  - 4 row circular-finned heat exchanger



- Single row plate-finned heat exchanger





# Experimental Measurements on Prototypes

- Measurements carried out in Ireland
- Test facility to provide slightly superheated steam at approx. 1.5Bar



- Experimental arrangement was modified to facilitate air-side or steam-side testing

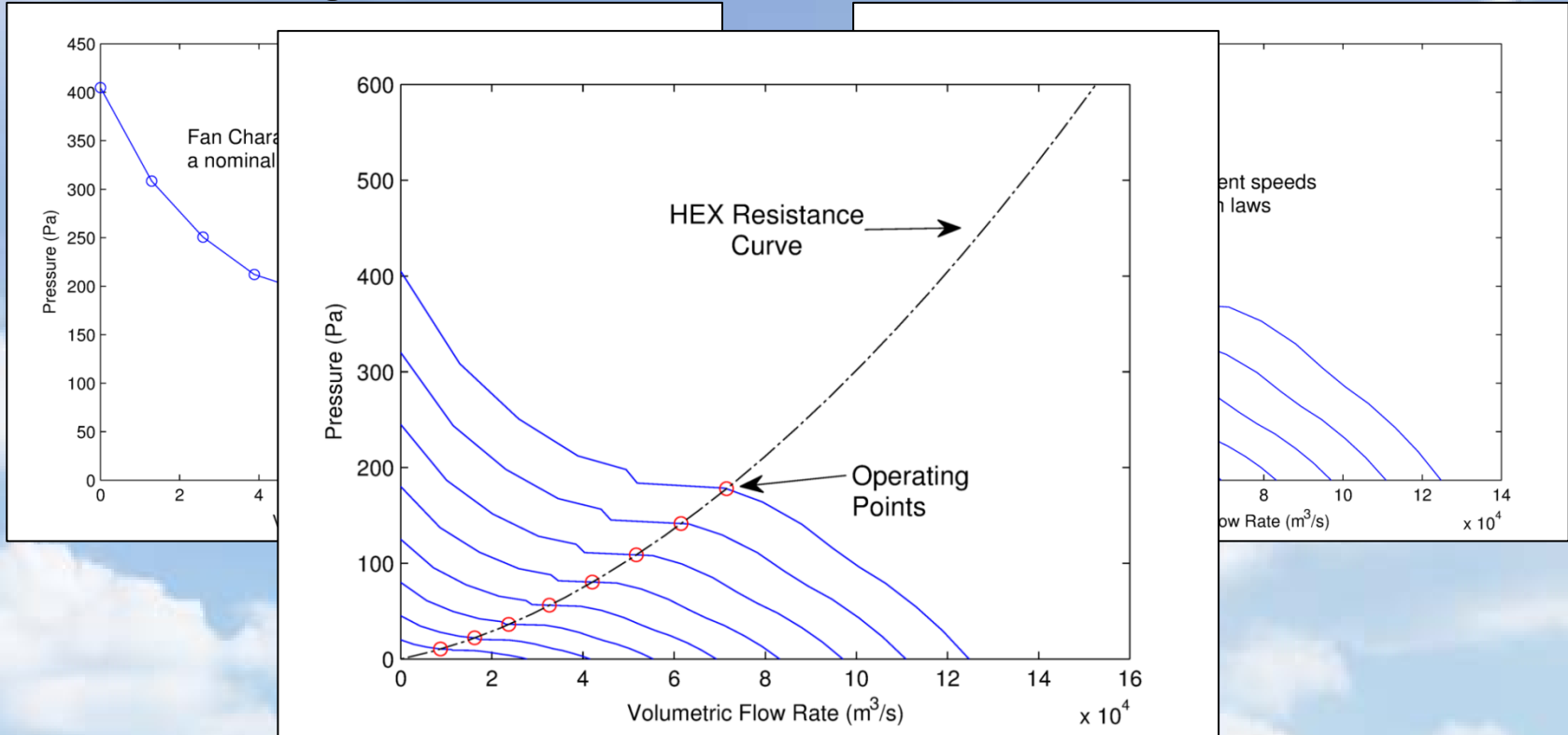


# Air-Side Characterisation of MACC

- Quantify aerodynamic and thermal performance of heat exchanger
  - Friction Factor (Pressure Drop)
  - Nusselt Number (Heat Transfer)
- Empirical correlations are available in literature to predict the performance of various heat exchangers
  - Theory cannot model the complex flow
  - Accuracy of correlations must be verified by experimental means
  - Verification provides confidence in correlations for use in optimisation techniques

# Air-Side Characterisation of MACC

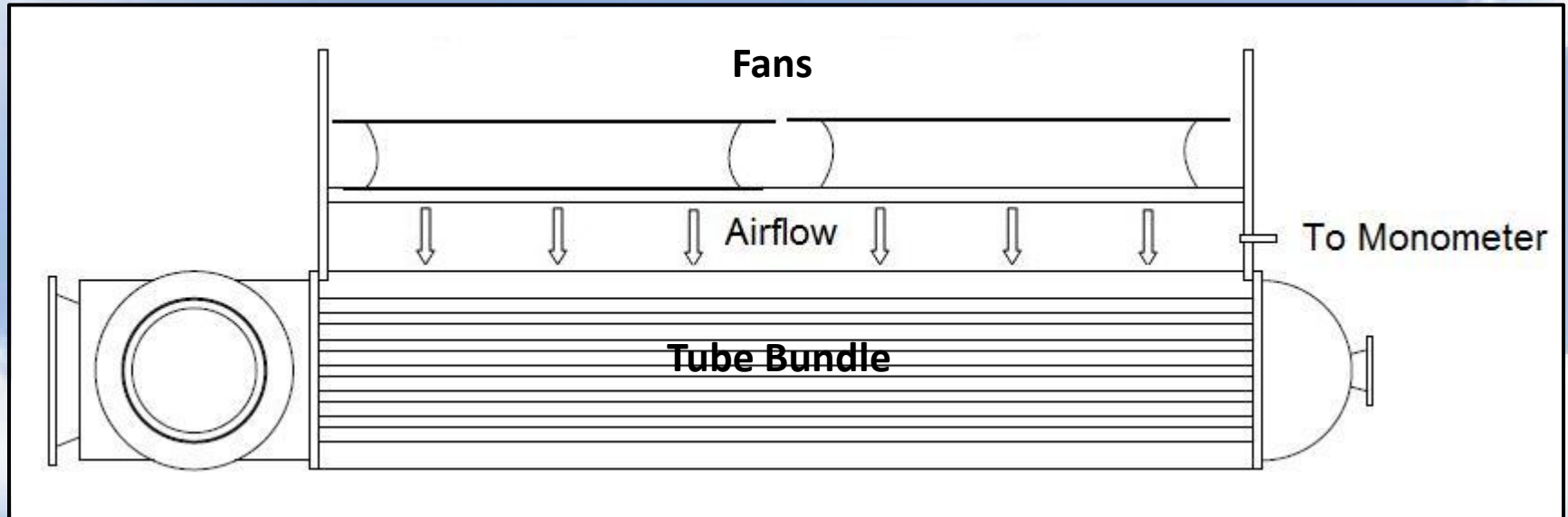
- Correlations are used to predict performance from interaction of fan and heat exchanger



- Intersection of fan curves & resistance curve  $\rightarrow$  HEX operating points
  - Flow rates (volumetric, mass, Reynolds number)
  - Pressure drop (friction factor)

**MACCSol** Nusselt number (air-side heat transfer coefficient)

# Air-Side Characterisation of MACC – Experimental Procedure (Pressure Drop)

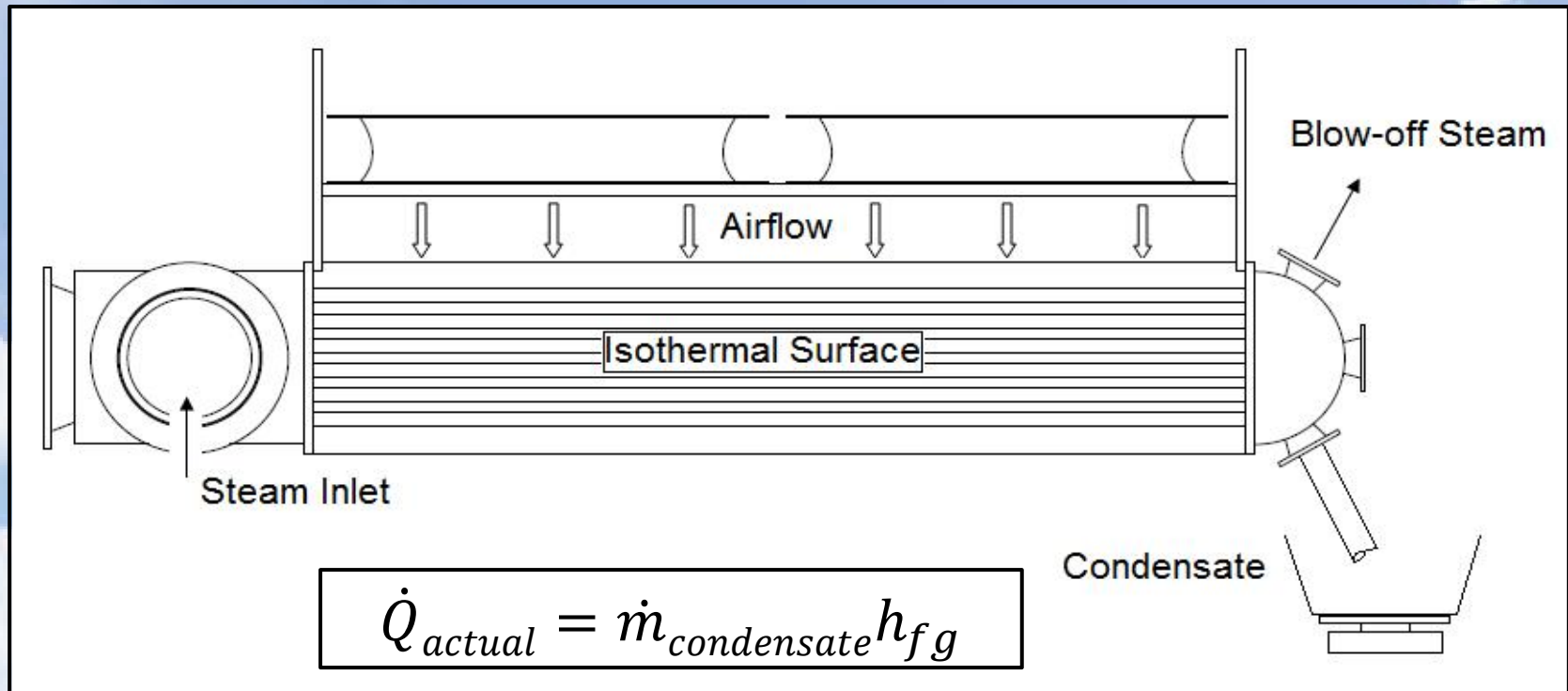


- Fan software to control and measure fan speed and power consumed
  - Vary fan speed incrementally from 100rpm to 1000rpm
- Digital manometer to measure pressure
  - Measures pressure differential between heat exchanger and atmosphere



# Air-Side Characterisation of MACC – Experimental Procedure (Heat Transfer)

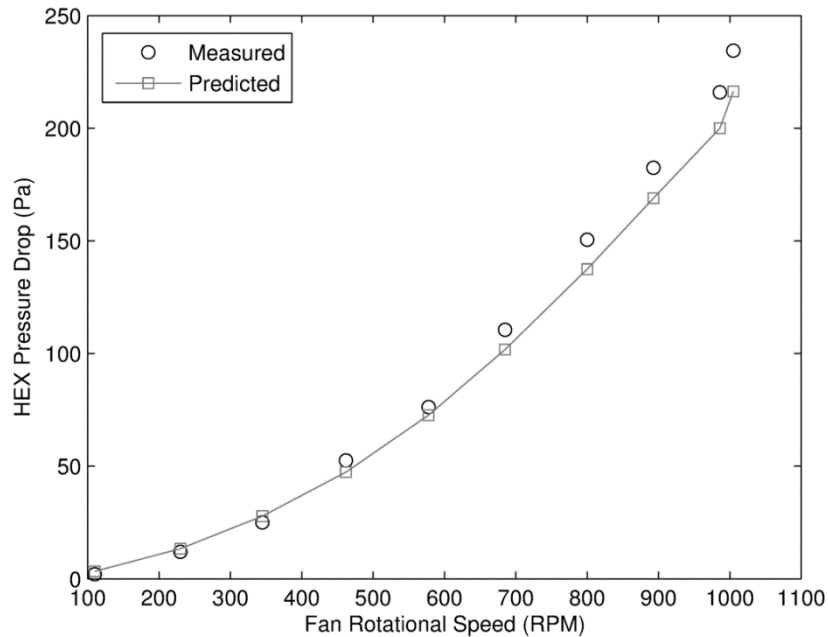
- “Kays and London” test method



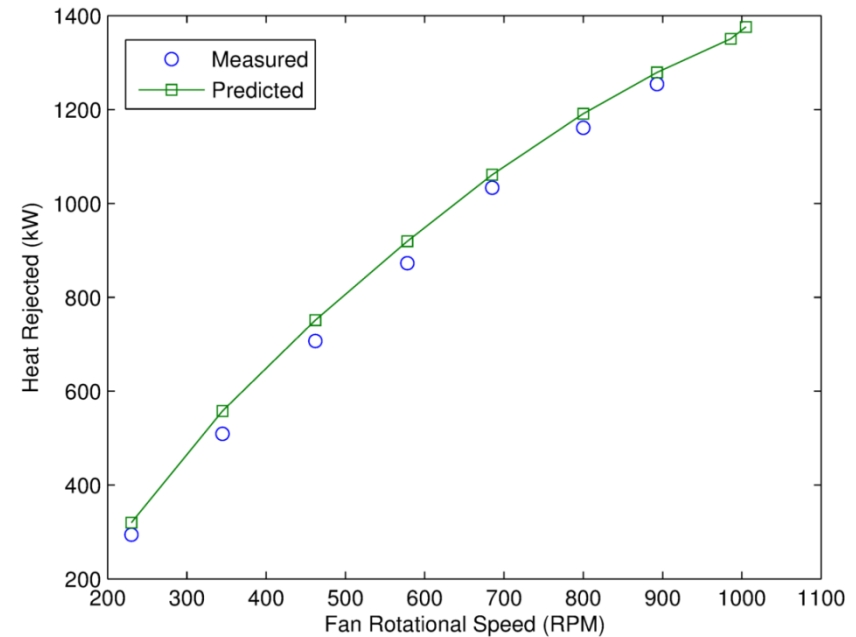
- Slightly superheated steam at inlet
  - Excess steam was forced through to minimise condensate resistance
  - MACC was inclined to promote condensate runoff

# Air-Side Characterisation of MACC – Experimental Results

## Pressure Drop



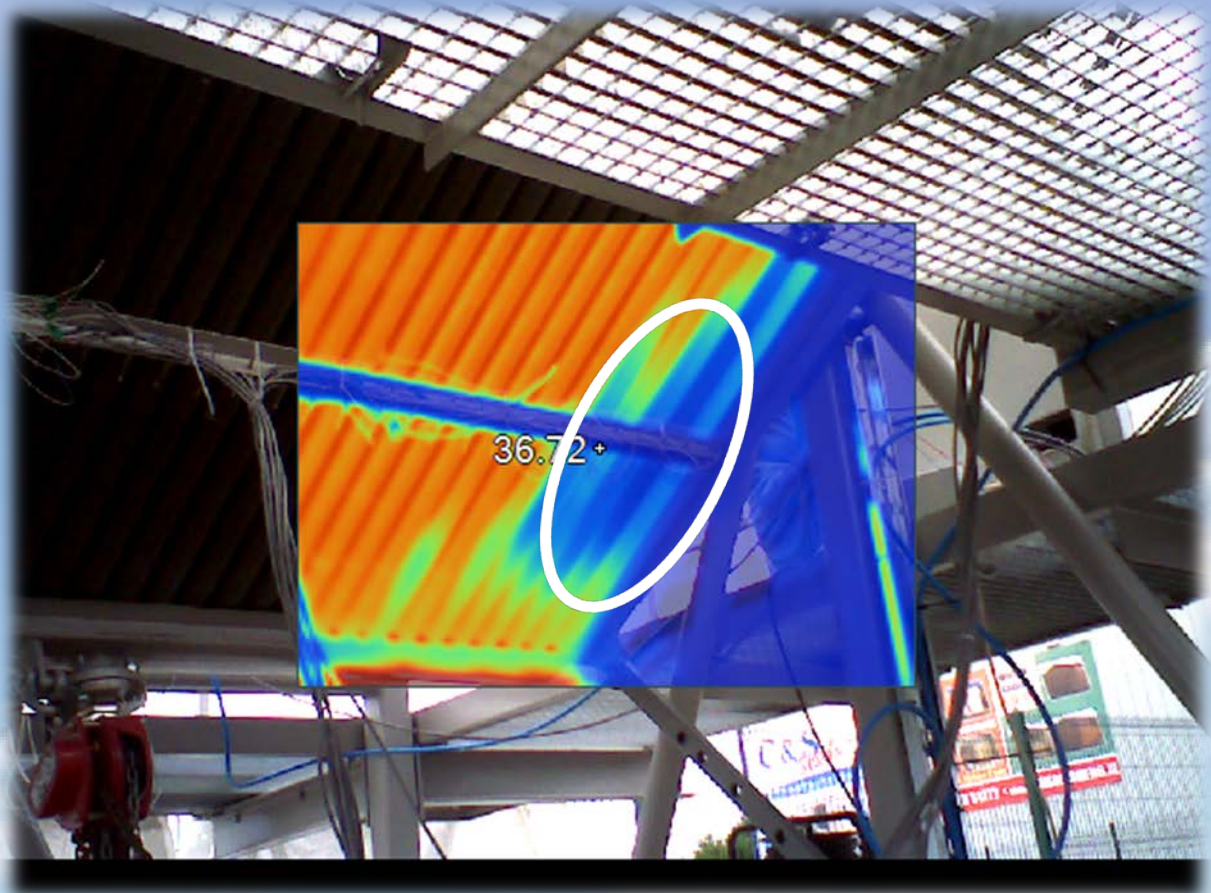
## Heat Transfer



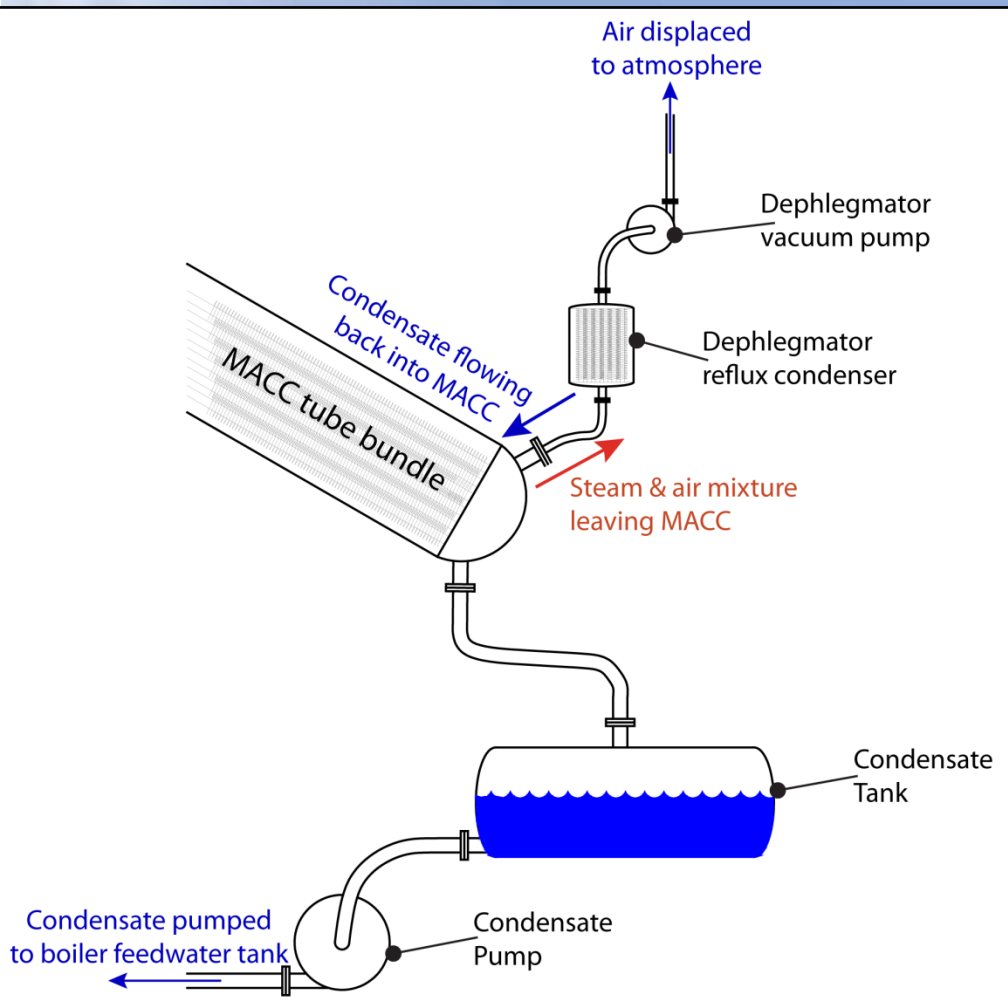
# Steam-Side Characterisation of MACC

- Quantify the thermal and fluidic performance of the MACC under operational conditions
  - Insight into how the MACC will perform in a power plant
  - Vacuum conditions
  - Air leaks
  - Air-side theory cannot adequately predict condenser performance with condensate-side phenomena such as air leaks, subcooling, etc.
- Backflow was an issue prominent in the multi-row designs
  - Coupled with air ingress, this lead to “*non-condensable blanketing*”



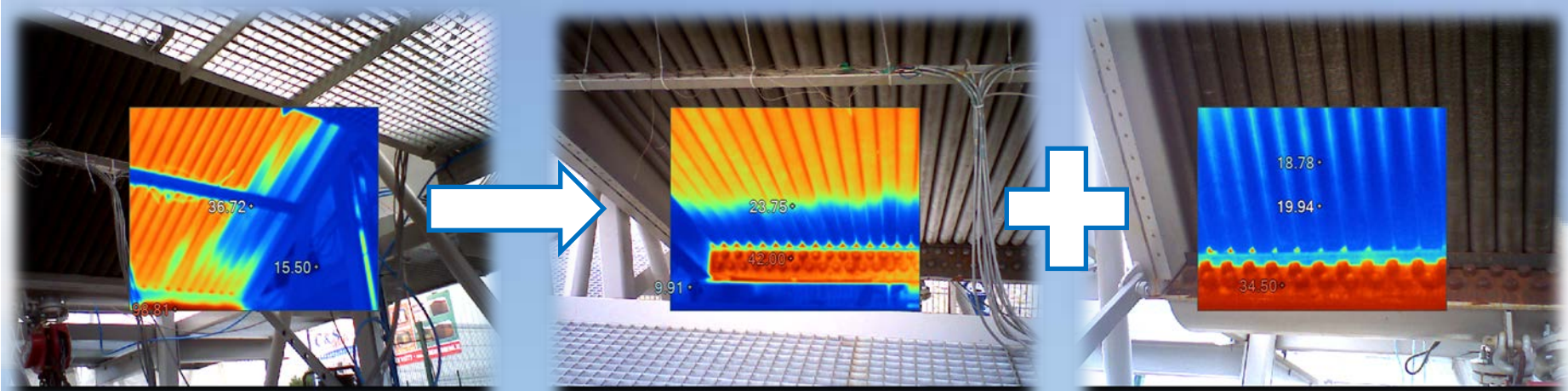


# Steam-Side Characterisation of MACC – Experimental Arrangement



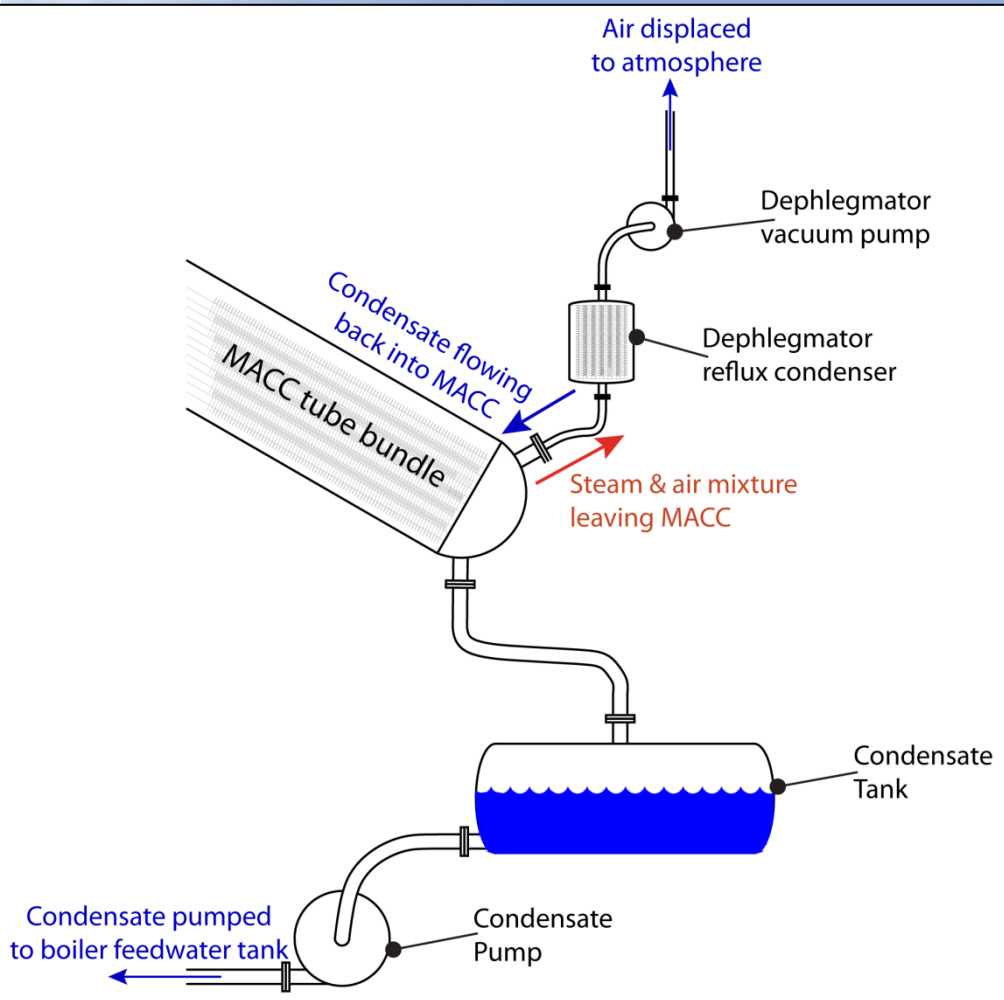
- Solution to air pocket formation – dephlegmator (secondary heat exchanger in series with MACC)
- Excess steam flows from common exit manifold into dephlegmator
- Condensate flows back into MACC exit manifold
- Air leaks are continually displaced by downstream vacuum pump to maintain vacuum

- Backflow is prevented
- Ensures effective heat transfer area is not reduced → Confidence to proceed with testing





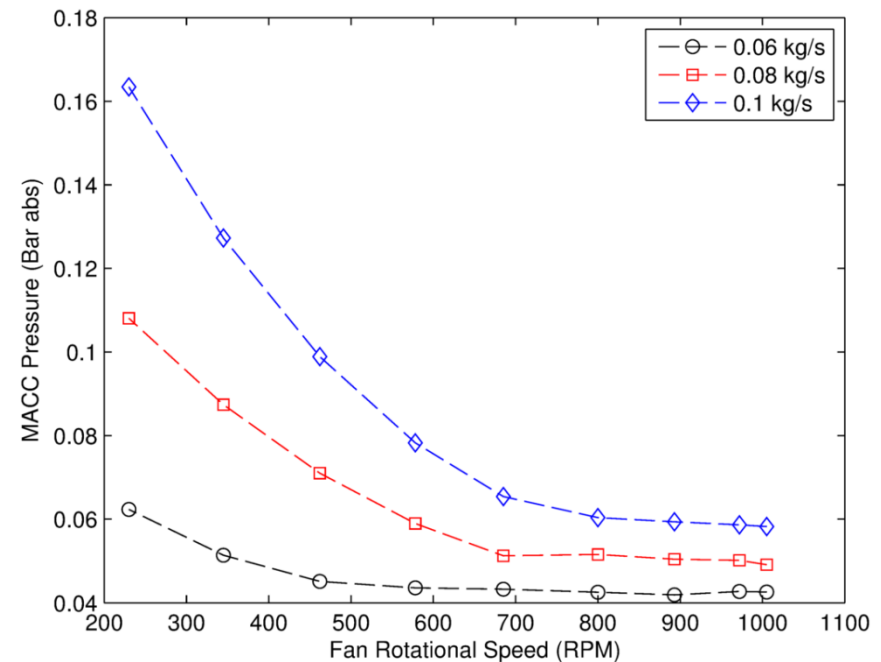
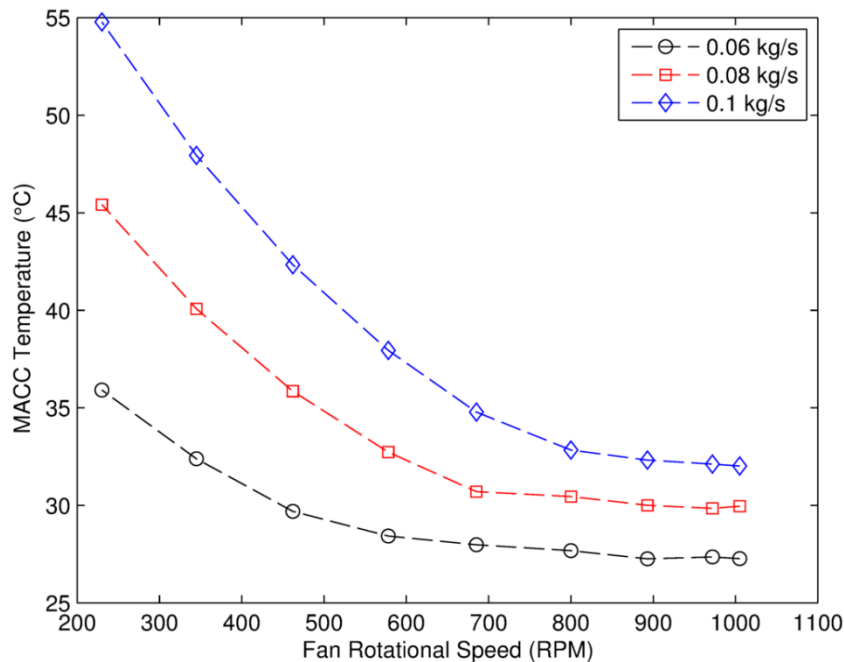
# Steam-Side Characterisation of MACC – Experimental Procedure



- Purge any air present at startup by forcing steam through tubes
- Confirm isothermal conditions
- Close system and turn-on fans to 1000rpm
- Turn-on vacuum pump and open system to dephlegmator
- Allow for steady-state vacuum
- Resume steam flow and incrementally decrease fan speed from 1000rpm in steps of 100rpm
- Measure variation in MACC temperature & pressure

# Steam-Side Characterisation of MACC – Experimental Results

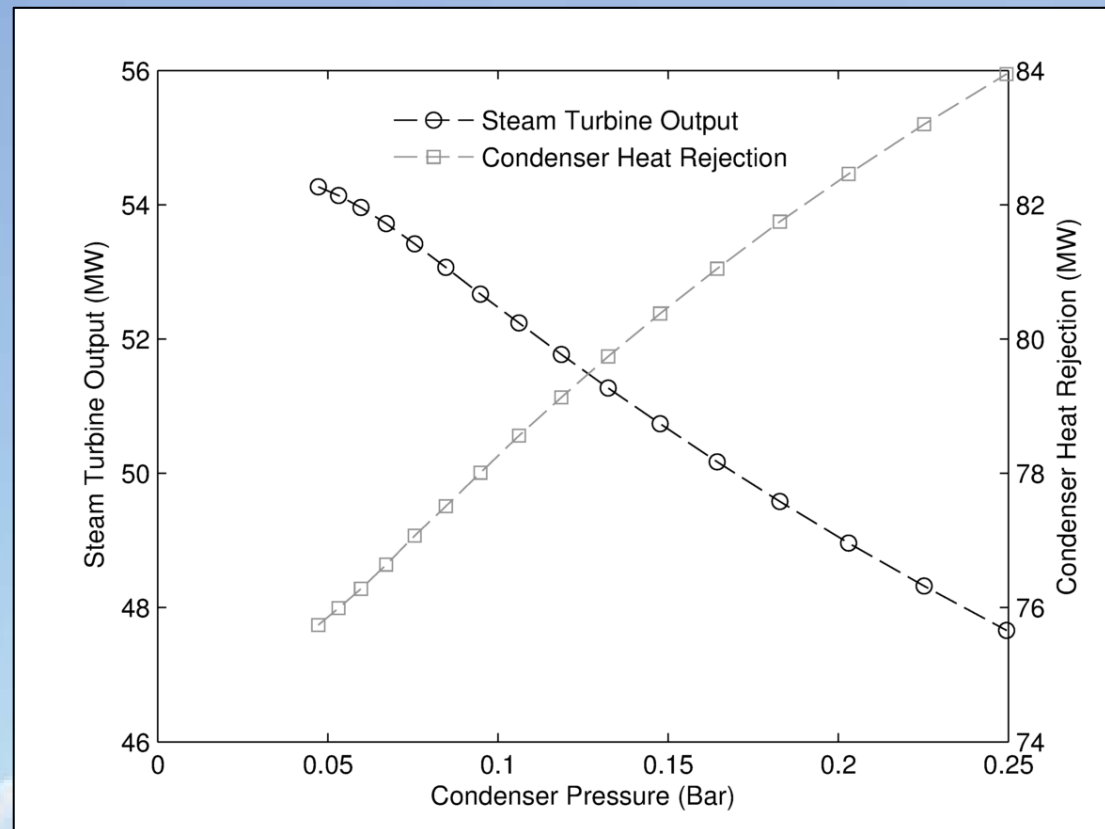
- Variation of temperature and pressure with fan speed for a range of steam flow rates



- Results are indicative of how the MACC will be capable of controlling the outlet of a steam turbine in a plant

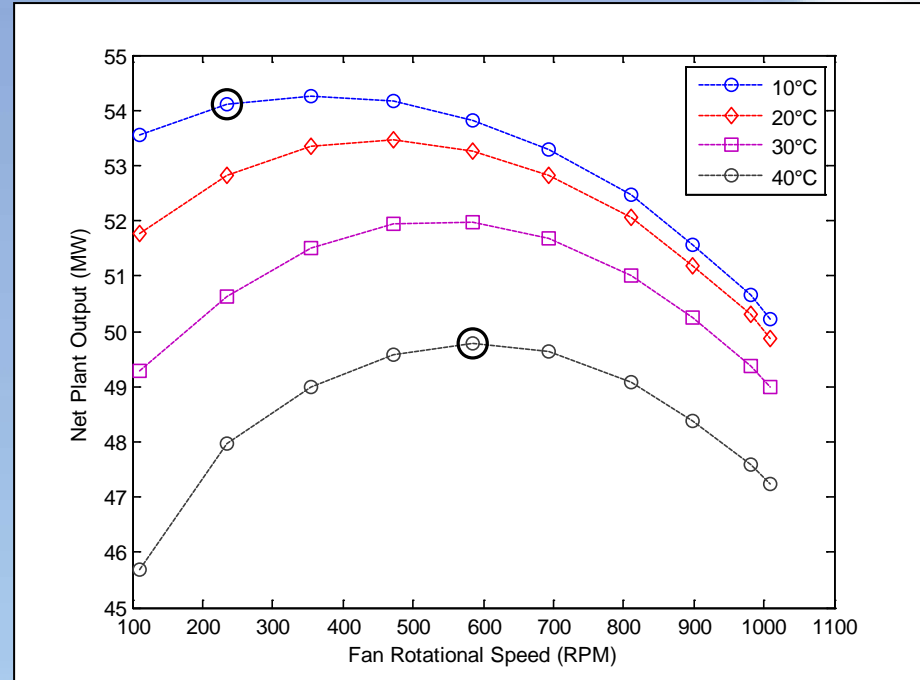
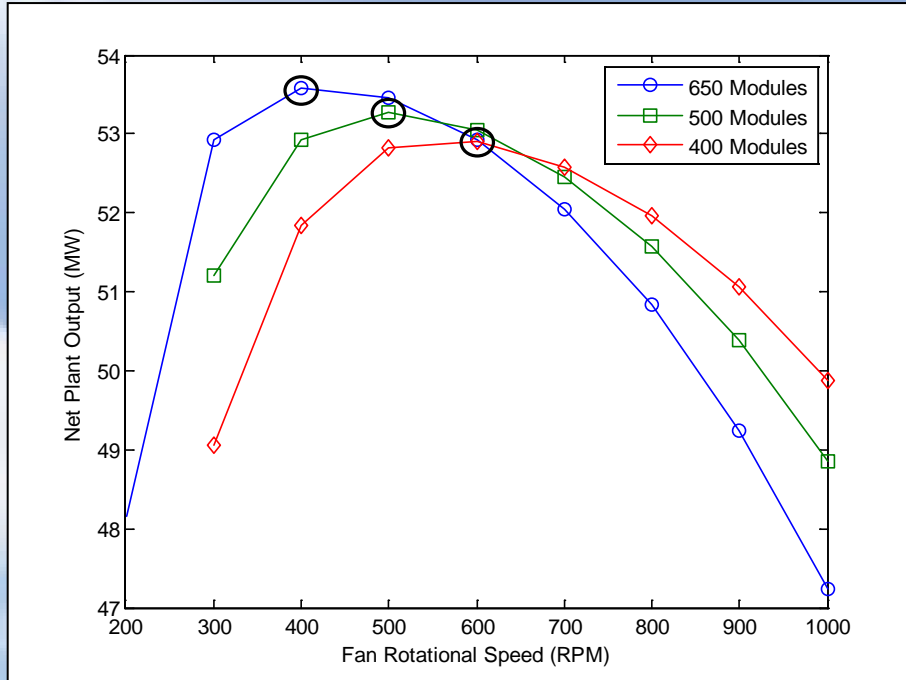
# Impact of MACC on Plant Output

- Determine the effect of installing MACC system on the output of a plant
  - 50MW steam turbine characteristics provided by project partner
- Only concerned with condenser-turbine relationship
- All other power block parameters such as turbine inlet temperature and flow rate were assumed constant





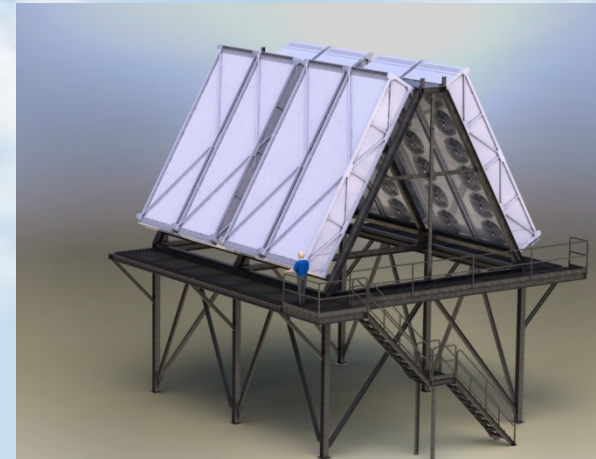
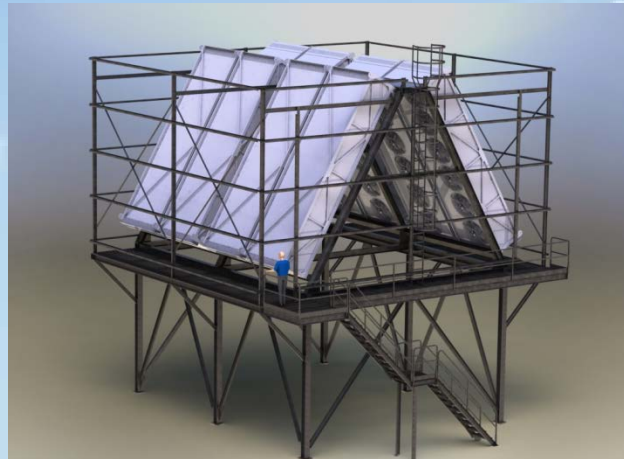
# Impact of MACC on Plant Output



By increasing fan speed from 200 rpm at 10°C to 600 rpm at 40°C, a 1.5MW loss is avoided

# Current Work

- “Demonstrator” MACC is being fabricated in Ireland and due to be shipped to CSP pilot plant in Australia
- 1.2MW central tower CSP plant
  - Owned and operated by Vast Solar (part of the *Australian Solar Institute*)
  - Will be operated for 18-24 months
  - MACCSol member will be present on site to monitor performance and record data



# The End

- Thanks for your time. Any questions/comments?



**MACCSol team members visiting Gemosolar  
“central tower” CSP site in Southern Spain**