



Howden Netherlands – Cooling Fans

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Revolving Around You[™]



STORK®

1955	Ventilatoren Stork Hengelo starts production of aluminum Cooling Fans
1960	The company adopts Fiberglass Reinforced Polyester for its Cooling Fans
1989	Howden takes a majority interest in the fan division of Stork
1992	Ventilatoren Stork Hengelo is acquired 100% by Howden and the company name changes to Ventilatoren Sirocco Howden (VSH)
2006	The company is renamed "Howden Netherlands" (HNL)







Specific features of Howden Cooling Fans

High air flow volume: to 3000 m³/s (6.5M ACFM) Low pressure drop : 350 Pa (1.5" WG)

Large diameter : 0,7 up to 21 m (3-60')

:

Temperature

Standard Optional : - 20 to 65 °C (-5 to 150F) - 60 to 135 °C (-75 to 275° F)





Air Cooled Heat Exchanger A.C.H.E

Air Cooled Condenser A.C.C.



Mechanical Draft Cooling Tower C.T.



Retrofit

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What is Retrofit?

More airflow = more cooling capacity

With retrofit we mean replacing a cooling fan in an existing cooling system for the purpose of:

- Plant Performance
- Efficiency
- Noise reduction



Retrofit possibilities are strongly enhanced by the use of (Ultra) Low noise fans.





Specific advantages of a cooling fan retrofit:

- Capacity can be increased quickly and easily on same footprint
- Sound emission (noise) reductions, crucial in field noise
- Efficiency increases
- The upgrade can be arranged in stages, no down time
- Low investment, short return on investment
- Possibility to prove the concept and ROI









Cooling Fan Theory

Fan Laws in Practical Applications



System resistance



Resistance



Fan Power (P)

- A fan is a mechanical device converting mechanical input power into aerodynamic power
- Aerodynamic power is the product between flow and pressure
- Cooling Fans are designed to provide large air volumes at low static pressure rises

$$P_{aero} = (Q \times P_{stat}) / _{stat}$$

$$P_{aero} = (Q \times P_{tot}) / tot$$





 $\Delta p = k \rho Q^2$

System Resistance and Fan Curves

- System resistance line
- Fan curve
- Stall Area
- Static Pressure **P**_{stat} in **Pa**





Pressure an Volume Margin

Pressure Margin API 661

"Fan selection at design conditions shall ensure that at constant speed the fan can provide by an increase in blade angle a 10 percent increase in airflow and a corresponding pressure increase. Since this requirement is to prevent stall and inefficient operation of the fan, the resulting increased power requirement need not govern the driver rating."



Pressure Margin Constant Blade Angle

Pressure margin value the fan can make for the set blade angle before stalling. This is a more realistic approach as pollution of the cooling unit with time will cause an increase in system resistance; the blade angle will not be adjusted.







Practical Facts of the Combined Fan Curves and System Laws (1)



Change in Resistance Curve

Change in Fan Speed



Practical Facts of the Combined Fan Curves and System Laws (2)





Fan Sizing – Fan Diameter





Fan Sizing – Number of Blades



					Inp	ut data							
Application	1		: Cooling tower										
Air flow		: 150	150.0 [m ³ /s]		Installation type Mounting orientation Fan inlet shape			: Ind	: Induced Draught : vertical shaft; hub at inlet : Bell. L/D = 0.15				
Static pressure Inlet temperature Air density Fan diameter Fan blade type Blade number			: 150	.0 IF				[Pa] [°C]					: ver
			: 20.0) [9									:Be
			: 1,200 [kg/r : 14 [ft]		kg/m³]	No diffusor present							
						Noo	bstacles	present					
			: ELF : All possible										
Fan tip spe	eed		: 45,0	45.0 [m/s]									
Fan clearance		:0,01 (2S/Fa		2S/FanDia)								
Crosswind		: 0,0	: 0,0 [m/		n/s]								
					Selecti	on result	5						
Fan typə	Тір	RPM	Blade	Static	Total	Fan shaft	pressure	Air flow	Total	Cf	Ср		
	speed		angle	efficiency	efficiency	power	margin	margin	PWL				
	[m/s]	[min^-1]	[1]	[%]	[%]	[kW]	[%]	[%]	[dB(A)]				
14 ELF 4	45,0	201,1	23,5	56,2	79,9	10,1	22,1	10,6	95,0	0,233	0,123		
14 ELF 5	45,0	201,4	20,9	56,9	81,0	39,5	36,3	16,8	95,0	0,233	0,123		
14 ELF 6	45,0	201,4	19,1	57.3	81,5	39,3	49,2	22,1	95,0	0,233	0,123		
14 ELF /	45,0	201,4	18,2	59,5	84,/	37,8	51.2	25.4	95.0	0,233	0,123		



Fan Sizing – Speed



smaller pitch - higher efficiency - lower power consumption - higher noise big pitch - low efficiency - high power consumption low noise – higher risk for stall



Fan Laws (1/2)

- $Q = Volume in m^3/sec$
- N = Speed in rpm
- D = Diameter in meter
- p = Air Density in kg/m3
- H = Static Pressure in Pa

Key essential to know for making fan assessments!

 $\frac{Q}{Q_r} = \left(\frac{N}{N_r}\right) \left(\frac{D}{D_r}\right)^3$

 $\frac{P}{P_r} = \left(\frac{N}{N_r}\right)^2 \left(\frac{D}{D_r}\right)^2 \left(\frac{p}{p_r}\right)$

 $\frac{H}{H_r} = \left(\frac{N}{N_r}\right)^3 \left(\frac{D}{D_r}\right)^5 \left(\frac{p}{p_r}\right)$

 $\frac{Q_2}{Q_1} = \frac{n_2}{n_1}$



Fan Laws (2/2)

Volume:



Abs. Power:

$$\frac{P_{Fan2}}{P_{Fan1}} = \left(\frac{n_2}{n_1}\right)^3$$

Noise:

$$\Delta PWL = 60LOG\left(\frac{y_2}{y_1}\right)$$

- *Q* Volume flow
- n Fan speed
- p Static pressure
- P Power consumption
- PWL Sound powerlevel



Choice of Fan Type with respect to Noise

Various Cooling fan options for an identical duty point.

Fan Diameter 8 meter 280 m³/sec 110 Pa

Difference in Noise generation up to 15 dB(A)

Shape	Noise reduction	Solidity	RPM	lipspeed	PWL	▲ dB (A)
	(((CS))) Standard	0,11	117	52	101	2
	(((I))) Low-noise	0,33	80	36	93	-7,5
	(((C))) Very low-noise	0,52	72	32	90	-10,5
	(((CSD))) Ultra low-noise	0,71	72	32	86	-15







Adjustment of the blade angle

Adjust blade angle

- Place a straight edge, which is at least as long as the profile width, on top of the discharge side of the blade at about 50 mm (2 inches) from the blade profile end (distance X).
- Place the inclinometer on top of the straight edge.
- Lift the blade at the tip and rotate the blade around its axis until the desired angle is set within a maximum tolerance of ± 0.5 degrees.



Fan Blade Tip Clearance



The tip clearance is the distance between the blade tip and the impeller casing. Howden recommends a tip clearance according to the applicable fan selection sheet. In general, the tip clearance is not constant around the impeller casing. This is because the impeller casing is not exactly circular.



CAUTION

The tip clearance must never be less than 0.25% of the impeller diameter!

Determine longest blade

- Measure the tip clearance (S) of all blades at a fixed point in the fan casing.
- 2. Determine the longest blade.



CAUTION

Do not measure at a split of the casing.

Measure tip clearance longest blade

- Slowy rotate the impeller manually to the various measuring points.
- Measure the tip clearance of the longest blade at the various measuring points. The number of measuring points = 12.

Note



If the the minimum tip clearance is too small, there are two options:

- The impeller shaft is not correctly centered. Refer to 5.1.3.
- Reducing the impeller diameter. Refer to 5.5.2.



Fan Tip Clearance adjustment



Install spacer rings

 Install one or more spacer rings (A) between the blade stem collars and the lower clamping pieces.



Note

The total thickness of spacer rings per blade equals the reduction in radius (= diameter/2) that is necessary to get enough tip clearance.



WARNING

The total thickness of the rings (X) must not exceed the value given in Table 1: "Maximum total thickness of the spacer rings".





Effects of Wind on FD fan

- Adds resistance and pressure loss
- Causes loss in fan performance
- Causes increased loading on the fan blades
- Recirculation (hot exhaust air flow back into the fan inlet)
- Reduced thermal performance









Non-uniform Inlet Flow due to Wind

20

20

40

40

60

80

Time (s)

100

120

140

160

180

• Separation from the inlet bell

15 r

10

0 -5 -10

-15 L

0.06

0.04

-0.02 -0.04 -0.06

dynamic blade loading [-]

air inlet velocity [m/s]

- Local reduction air inlet velocity
- Causes additional loading of the fan blades





Tips for making a good fan selection and assessment (1)

- Set the flow / diameter ratio to 7-11 m/sec air speed
- Choose application and possible recovery effects
- Set the air density
- Determine the pressure and obstacle influences (Noise and Pressure Loss)
- Set inlet shape
- Determine the desired pressure margin
- Check for mechanical frequency excitations
- Specify the maximum PWL of the fan

	0000.000/100000			_	1949 - 1949 - 1949	7467 197				
Fan Data 36	DVM8:				Application	on Data:				
Type: 30 Diameter: 30 Blades: 8 Discussion		16DVM8		:	Application: Draught: Mounting orientation:		Air Cooled Condensor Forced Draught Vertical shaft; hub at			
Blade angle: 2 Fan Static Efficiency: 5 Mass: 1 Moment of inertia: 1		:1,3 ⁻ i9 % I952 kg 5573 kg.m ² Input data - ◀			Inlet shape: Duct height: Tip clearance: Diffuser: Obstacles: Inlet fontal area: Inlet obstacle distance: Outlet fontal area: Outlet obstacle distance: Crosswind: Resistance exponent:		0,0 m 0,35 % n.a. 0,10 0,15 0,10 0,15 0,0 m/s 2			
Operating C	Conditions:			-1	Acoustic	al Data:			input data	• •
Alations		600 4 ml/s			1	and the State of the				
Airtiow:		000,1 m-/s		111	Inlet shape:		91,0 dB(A)			
Pressure reco	overy:	0% 04.0 Pa		111	Inlet obstacles:		0.8 dB(A)			
Static pressu	re:	94,0 Pa		1	Outlet obstacles:		0,6 08	(A)		
Recovery:	0,0 Pa C	utlet obstacles:	0,0 Pa	- 11	Outlet obstacles:		0,4 GB(A)			
Inlet shape: Inlet obstacles:	Inlet shape: 0,0 Pa Diffus Inlet obstacles: 0,0 Pa Cross		0,0 Pa 0,0 Pa		Lw(A) fan total: 92,2 dB(A) Tolerance on Lw(A) fan total ± 2 dB					
mernegni.	0,0 Pa			- 11	Fan sound p	ower spect	rum:			
Fan Static Pressure: Fan speed: Tip speed:		94,0 Pa 55,5 rpm 31,9 m/s		•	Octave [Hz]	PWL [dB]	PWL [dB(/	A)] [dE	lerance 3]	
Fan shaft power:		110,1 kW		- 11	63	96,1	69,9	5		
Fan shaft torque		18958 Nm		- 11	125	96,1	80,0	3		
Airflow margi	n:	10.2	27.5	- 11	250	92,1	83,5	2		
Pressure mar	ain:	21.4 1 3	30.8	- 11	500	89,1	85,9	2		
1) according to A	PI 2) at selecter	d blade angle	50,0	- 11	1000	86,1	86,1	2		
Air density	1911 C	1 200 kg/m	2		2000	78,1	79,3	2		
Air density:		25.0 °C		211	4000	74,1	75,1	2		
mer tempera	ure.	20,0 0		1 I	8000	70,1	69,0	2		
Axial thrust:		11715 N			In(A) 1m he	eide inlet		63 1 dB/A		
Force loss of	1 / 2 blade(s):	15355 N / 28373 N			Lp(A) Im below inlet at 45°.			65.9 dB(A)		
Imbalance (IS	O 1940/1 G6.3)	: 71 N			Lp(A) 1m below inlet at 45":			71 0 dB(A)		
Fan rotation f	requency:	0,9 Hz			Lp(A) 1m be	ove cooler		67 7 dB(A)		
Fan operating natural freq:		3,4 Hz		- 11	EP(A) mia	ove cooler.		01,1 UD(A)		
Blade passing	7,4 Hz									
biade passing nequeiney.			100 March 100 Ma							



Blade passing frequency

+ Delts

Delta

m = 2

m = 1

60

Operating point

50

Tips for making a good fan selection and assessment (2)



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At the heart of your operations

Questions?



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